



Our mission:
Prevent Accidents
Reduce Injuries
Save Lives





















Michael Graham



Bruce Landsberg



Robert Sumwalt



Jennifer Homendy



Thomas Chapman

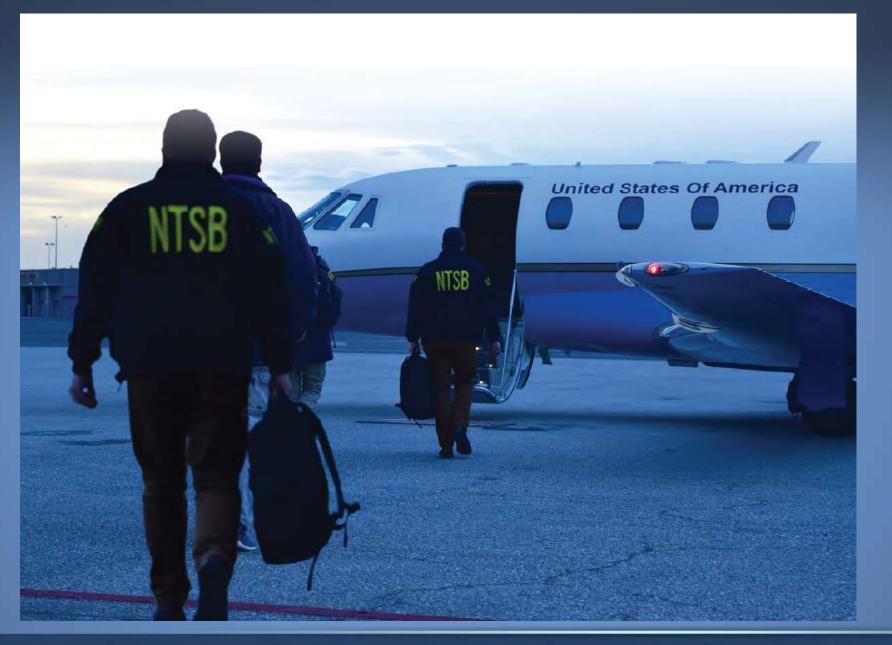




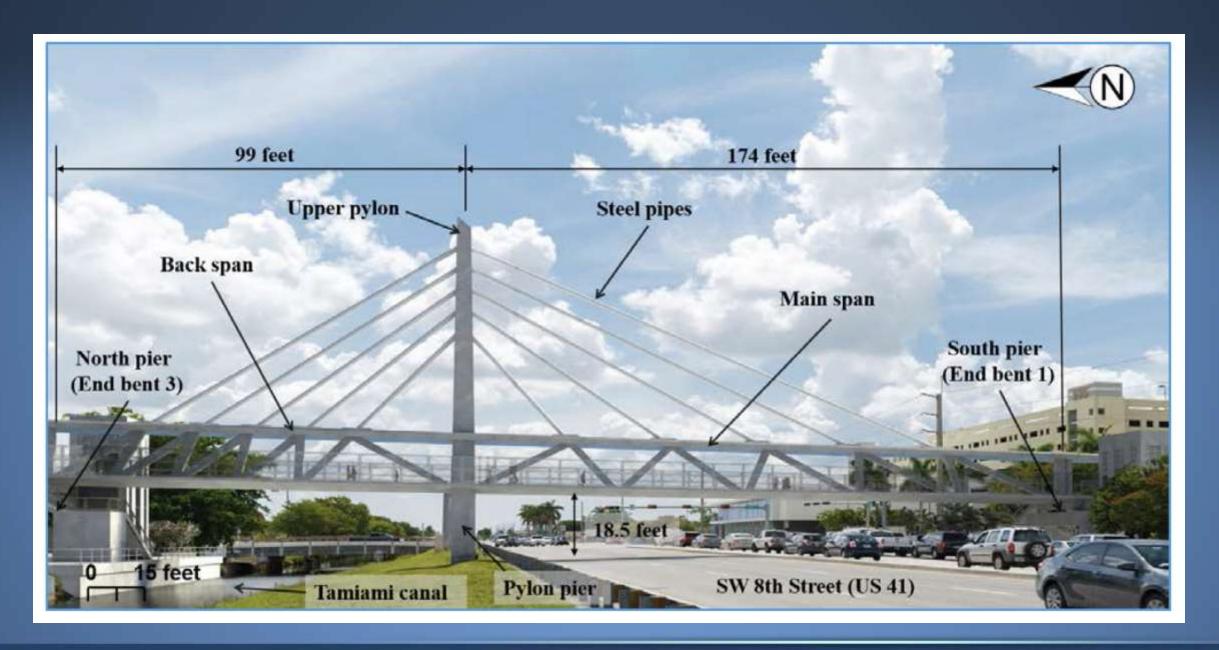
NTSB Response Operations Center









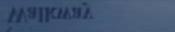




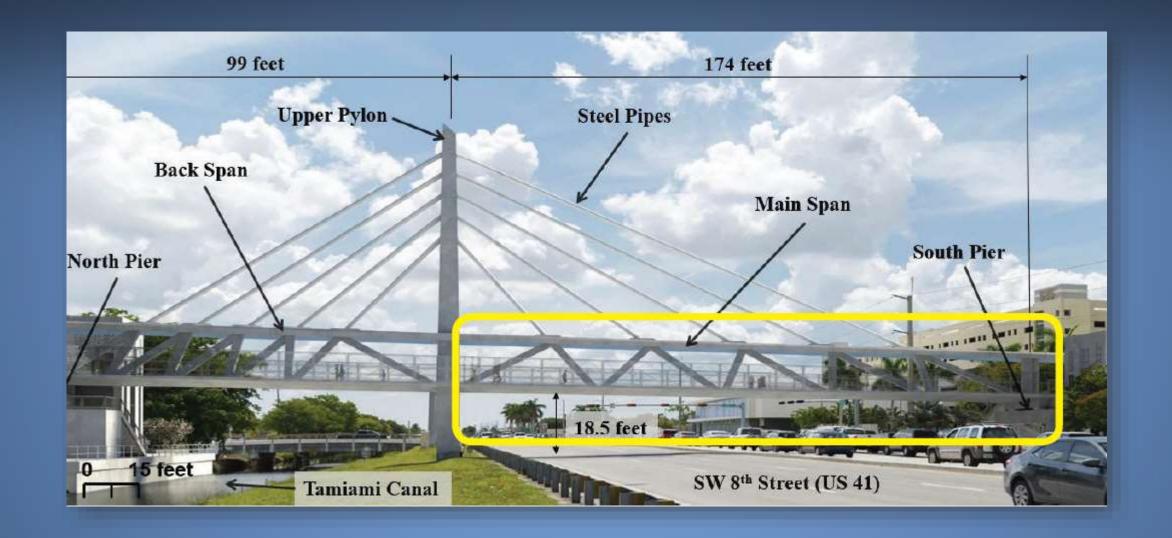










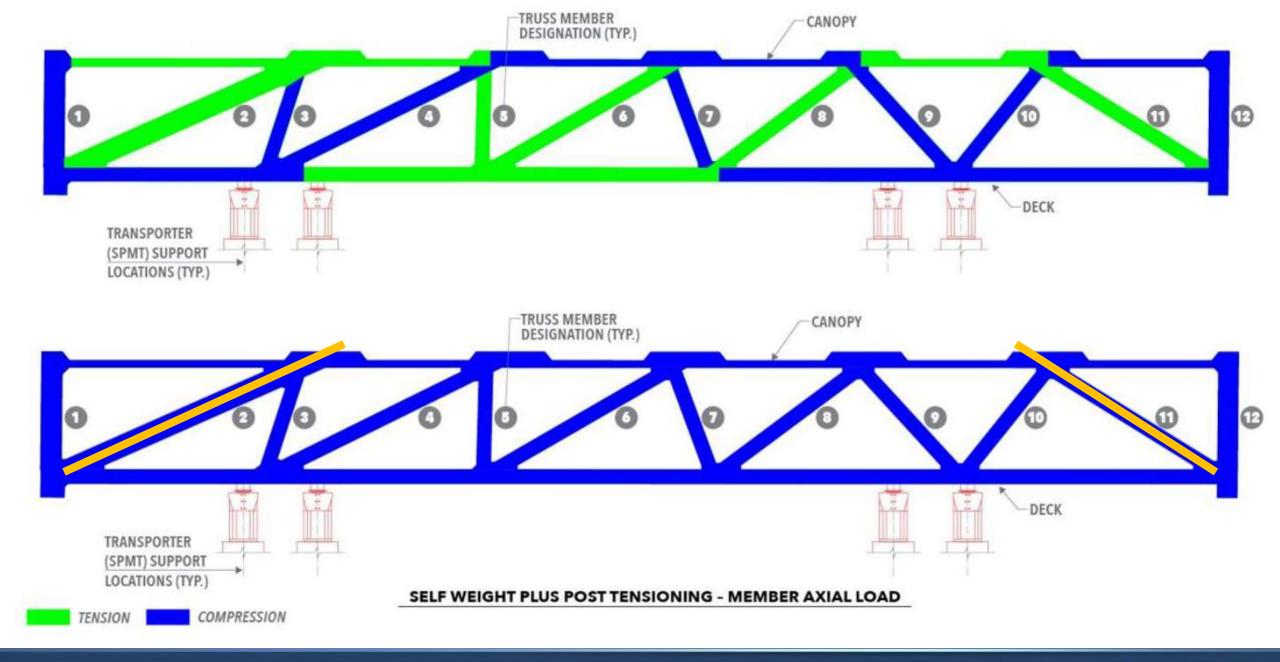




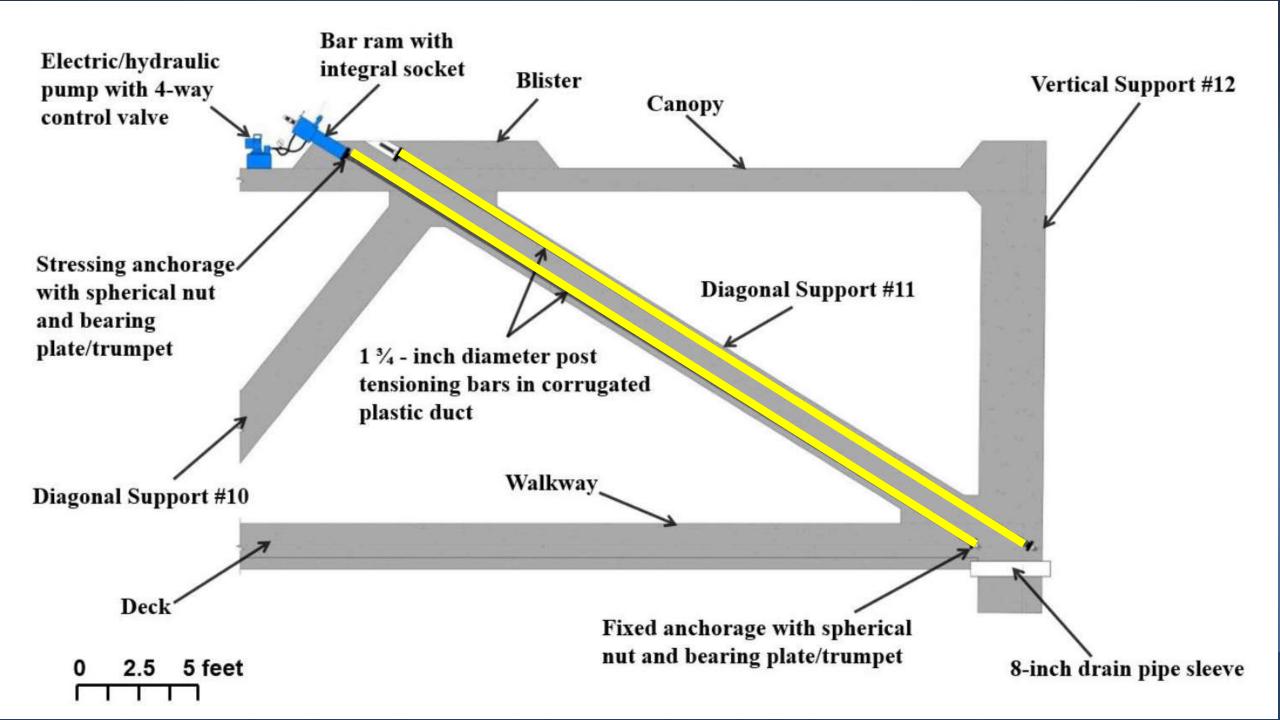
Accelerated Bridge Construction













March 10, 2018





March 15, 2018



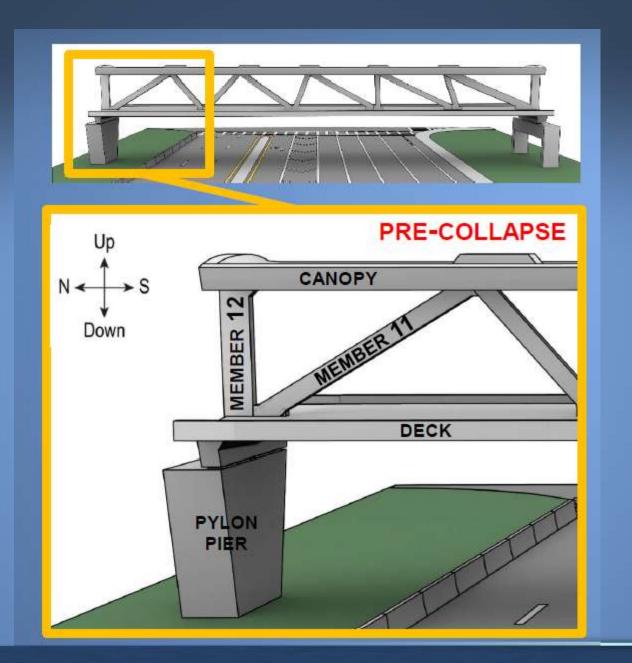


Facing East









Facing East





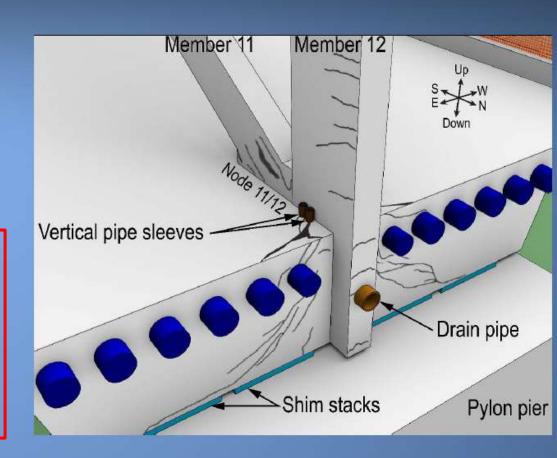
- Concrete Tested compressive strength and tensile behavior.
- Steel PT bars and rebar tested yield and tensile strength, and percent elongation.
 - Analyzed chemical composition of PT rods.

All material specimens were within specifications.



Cracking in Member 11/12 Nodal Region

- Structure showed notable cracking of reinforced concrete
- Extensive and large cracks in member 11/12 should have been recognized as abnormal
 - Cracks up to 0.016 inch wide considered acceptable
 - Structural cracks in bridge were up to 0.75 inch wide 40 times larger than typically acceptable
- Scale of cracking clear indication that load- resisting mechanisms were failing















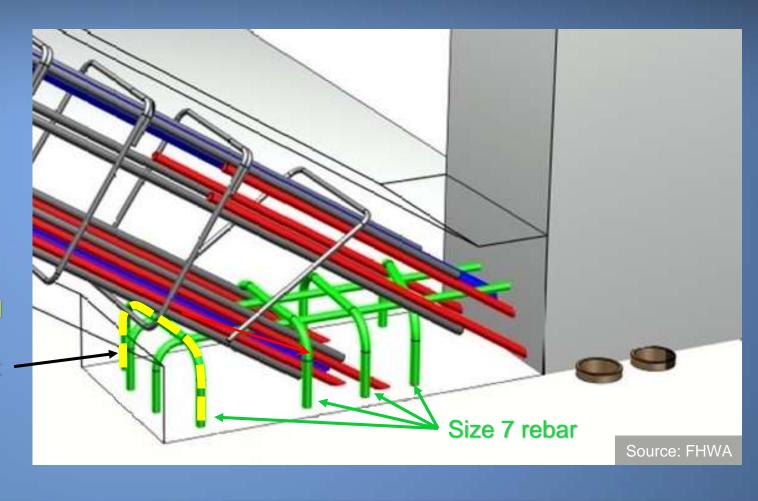


First Signs of Structural Distress

Portion of crack
 bypassed 25% of reinforcing steel at base of member 11



Crack passed above the southernmost two size 7 rebars





Date	Time	Communication Method	Response
March 13	9:45 a.m.	Email from FIGG design manager to MCM	"We do not see this as a safety issue"
	4:13 p.m.	Voice mail message from FIGG EOR to FDOT	"But from a safety perspective, we don't see that there's any issue there, so we're not concerned about it from that perspective"
	5:18:22 p.m.	Email from FIGG design manager to MCM	"Again, we have evaluated this further and confirmed that this is not a safety issue"
March 14	10:50 a.m.	Email from MCM to Structural Technologies	"FIGG has further evaluated and confirmed that the cracks encountered on the diaphragm do not pose a safety issue and/or concern"
March 15	9:00 a.m.	Presentation by FIGG EOR at meeting with FDOT; FIU; MCM; Bolton, Perez (and others)	"And, therefore, there is no safety concern relative to the observed cracks and minor spalls"
		Meeting minutes prepared by Bolton, Perez	"FIGG assured that there was no concern with safety of the span suspended over the road"
		Meeting minutes of March 15 prepared by FIGG	"Based on the discussions at the meeting, no one expressed concern with safety of the span suspended over the road"



Conclusion

- Based on conservative calculations, it is concluded that the design meets LRFD strength requirements for this temporary condition ...
 - And therefore the is no safety concern relative to the observed cracks and minor spalls









NTSB CHAIR: NTSB HAS BROUGHT A FULL INVESTIGATIVE TEAM

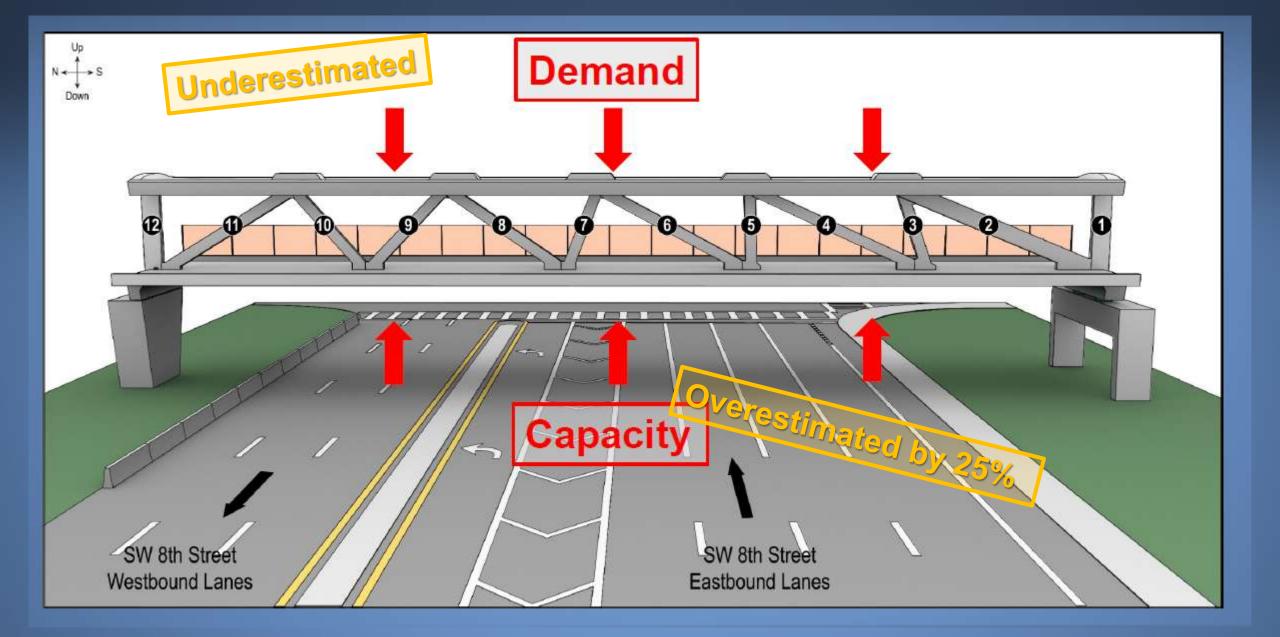
FOX NEWS ALERT



Critical Errors

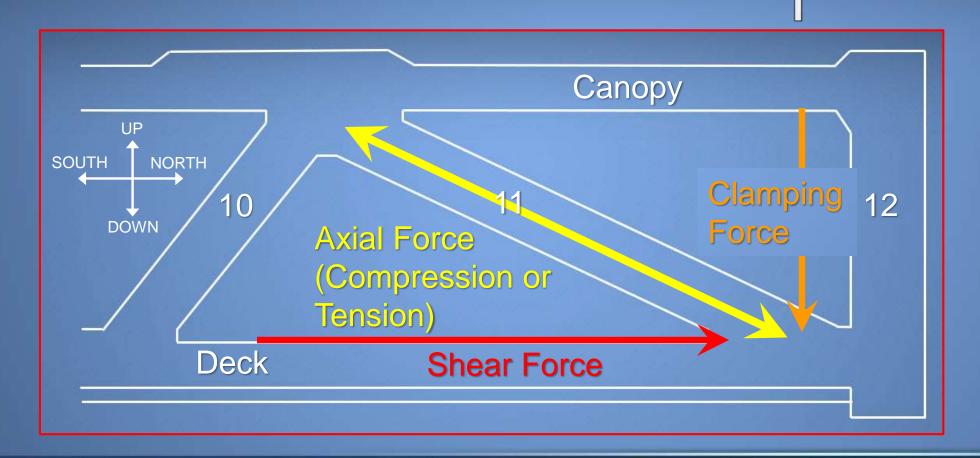
- Bridge was under-designed
- Peer review was insufficient
- Failure to close bridge to traffic and workers







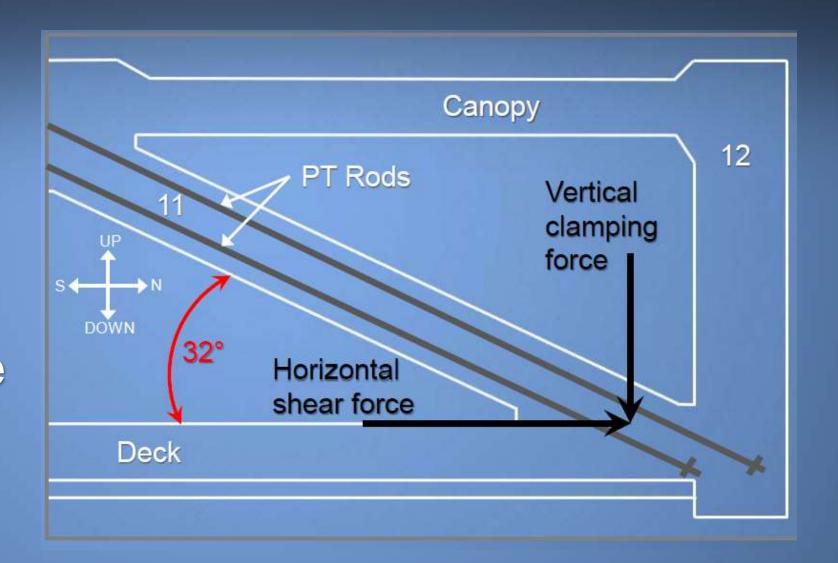
Forces on 11/12 nodal region





Magnitude of horizonal force — 60 percent larger than vertical force

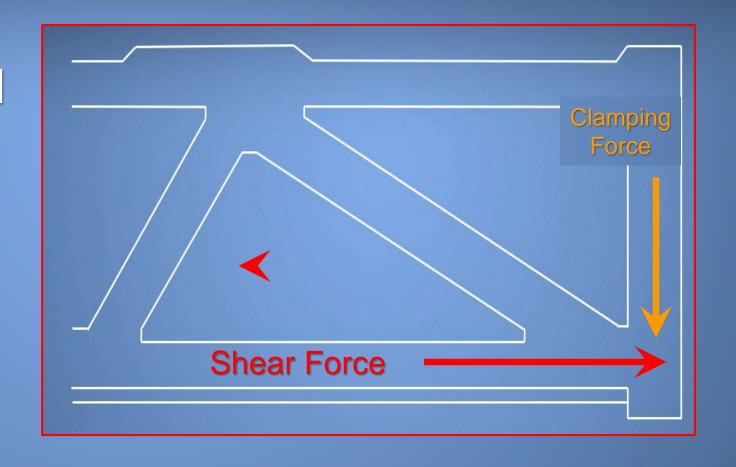
Facing West





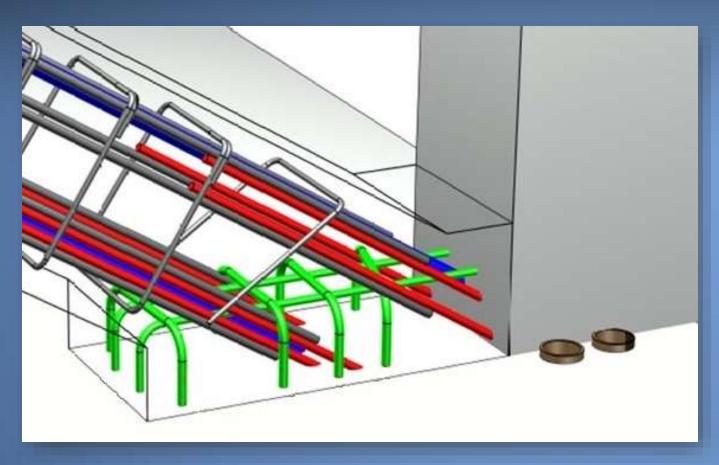
Interface Shear Demand

Figg underestimated interface shear demand at nodal region 11/12 by 46%.





270 percent more rebar needed



- Member 11 needed
 18 square inches
 cross sectional area
 of rebar.
- It only had 4.8 square inches.



Summary

- FIGG design made significant errors in determination of loads
- Chose the wrong interface shear demand value
 - Led to a severe underestimation of demand
- Chose the wrong load factor in calculating the permanent compression loading, or $P_{\it C}$
 - Led to a significant overestimation of capacity



The National Transportation Safety Board (NTSB) determines that the probable cause of the Florida International University (FIU) pedestrian bridge collapse was the load and capacity calculation errors made by FIGG Bridge Engineers, Inc., (FIGG) in its design of the main span truss member 11/12 nodal region and connection to the bridge deck. Contributing to the collapse was the inadequate peer review performed by Louis Berger, which failed to detect the calculation errors in the bridge design. Further contributing to the collapse was the failure of the FIGG engineer of record to identify the significance of the structural cracking observed in this node before the collapse and to obtain an independent peer review of the remedial plan to address the cracking. Contributing to the severity of the collapse outcome was the failure of MCM; FIGG; Bolton, Perez and Associates Consulting Engineers; FIU; and the Florida Department of Transportation to cease bridge work when the structure cracking reached unacceptable levels and to take appropriate action to close SW 8th Street as necessary to protect public safety.





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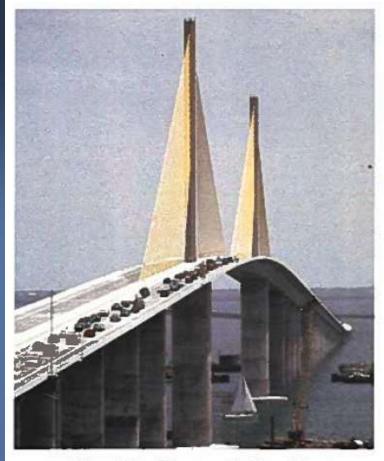


OYER BRIDGES

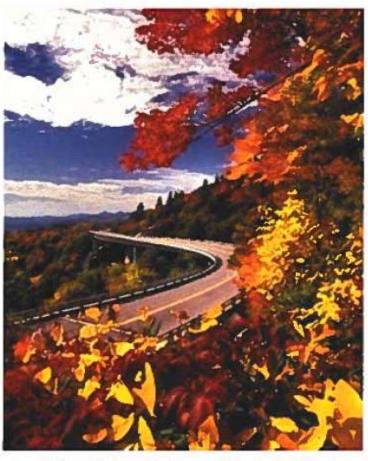
42 States 6 Nations

Brazil Columbia Guyana Canada India Saudi Arabia

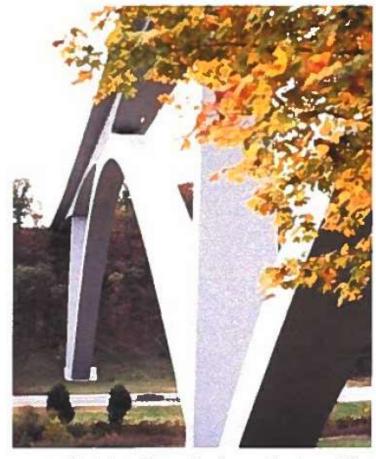




Sunshine Skyway Bridge, FL



Blue Ridge Parkway Viaduct, NC National Park Service



Natchez Trace Parkway Arches, TN National Park Service

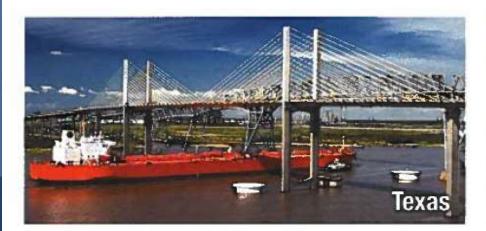
3 Presidential Awards

through the National Endowment for the Arts
-US Presidents gave 5 of these awards for Bridges-



FIGG Has Delivered More Concrete Cable-Stayed Bridges than any Firm in America

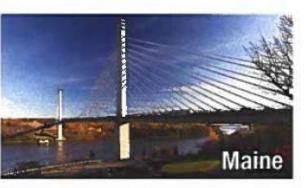
- 14 built concrete cable-stays in U.S.
- 12 FIGG responsible charge
 - 7 Engineer of Record -A first for each state
 - 5 Precast concrete -Engineer of Record For All of them



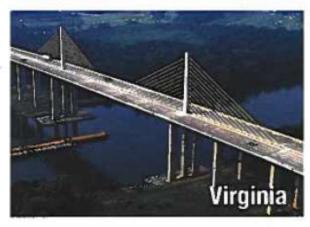












BRIEF

TxDOT seeks removal of FIGG from \$800M Harbor Bridge design



Designer FIGG Removed From One Bridge Job, Faces Scrutiny on Second





FIGG Presentation on Day of Collapse

Conventional Method

Rectangular Beam Analysis

Data:

- Section dimensions b, h, d, (span)
- Steel area As
- · Material properties f'c. fy

Required:

- · Nominal Strength (of beam) Moment Mn
- · Required (by load) Design Moment Mu

Total Nodal Shear Stability

V_{ni} =
$$cA_{cv} + \mu (A_{vf}f_y + P_c)$$

= 1360 kips

• c x Acv 57.6 k/sf x 23.62 sf

= 1908 kips • Mu x As Fy = 1.4x22.72x60 = 730 kips

= 3947 kips Total = Vni • Mu x Pc = 1.4 x 520 kips

 FIGG's general preference is to neglect the Cohesion portion when practical. Thus, Vni without "C" = 2638 kips

- · Phi = 0.9
- Phi)(Vni) = 3552 kips with "c"
- (Phi)(Vni) = 2374 kips without "c"

Conclusions and Recommendations

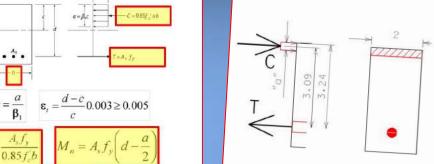
 The diagonal type cracks, in excess of FDOT criteria, should be sealed with approved methods and materials (Epoxy injection, etc.)

ntrolled)

≥ Mu

- The spalled areas have not been replicated by the engineering analyses. However ...
- The spalled areas are minor and it is recommended that they be prepared using normal procedures and poured back along with the up coming "pylon diaphragm" pour (different from and prior to the

Bending Check - Beam Theory



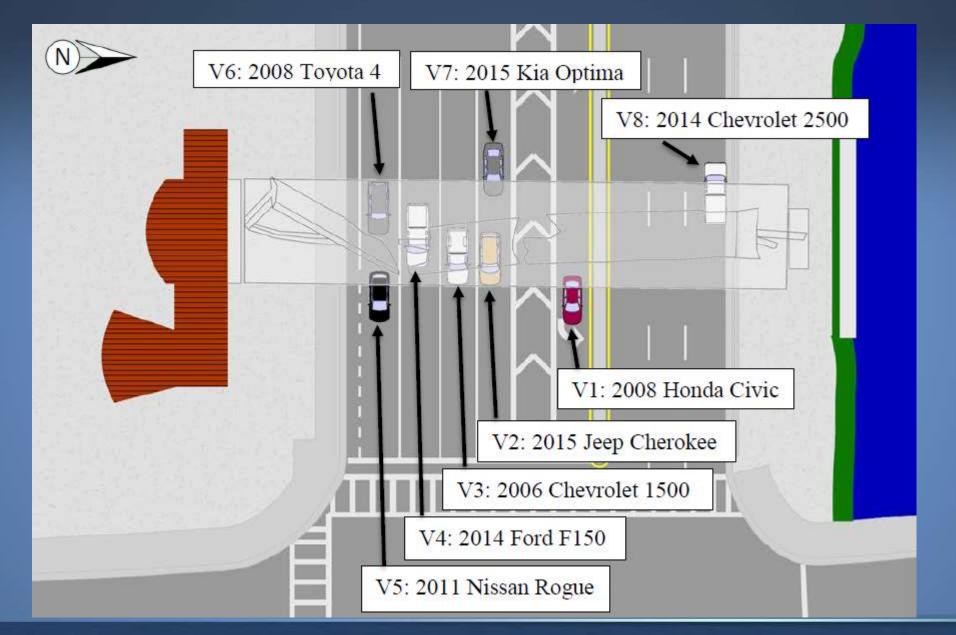
- Steel Area = 13.1 in^2
- T = (13.1)(60 ksi) = 786 kips
- f'c = 8.5 ksi = 1224 ksf
- (a)(.85 f'c)(b) = C = 786 kips
- Solving, "a" = 0.38 ft
- Mn = (T)(d -(a/2)) = 786x3.09' = 2398 kip-ft (nominal capacity)
- Phi = 0.9, so (Phi)(Mn) = 2158 kip-ft
- Which is larger than Mu = 2015 kip-ft
- · Check OK

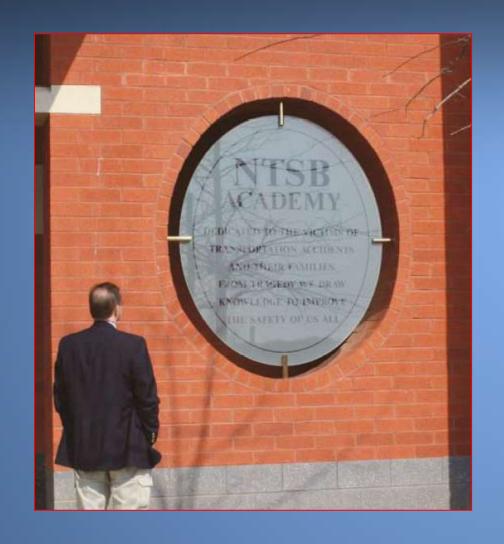
Conclusion

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And therefore the is no safety concern relative to the observed cracks







"From tragedy we draw knowledge to improve the safety of us all."





| National | Transportation | Safety Board